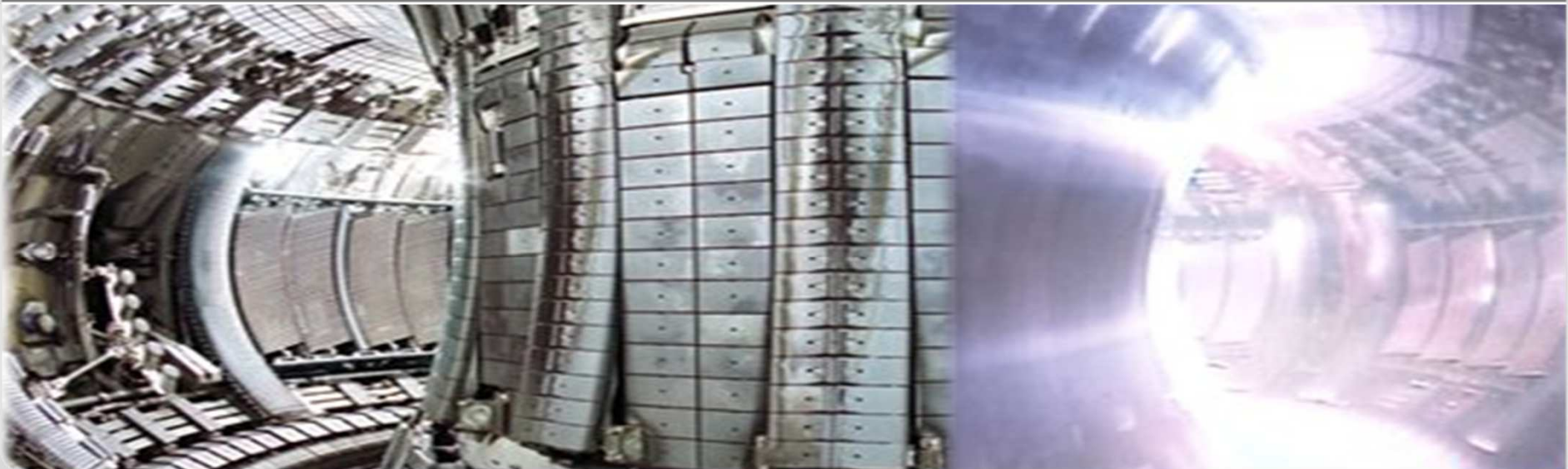


# ODS Steels and their behavior under neutron irradiation

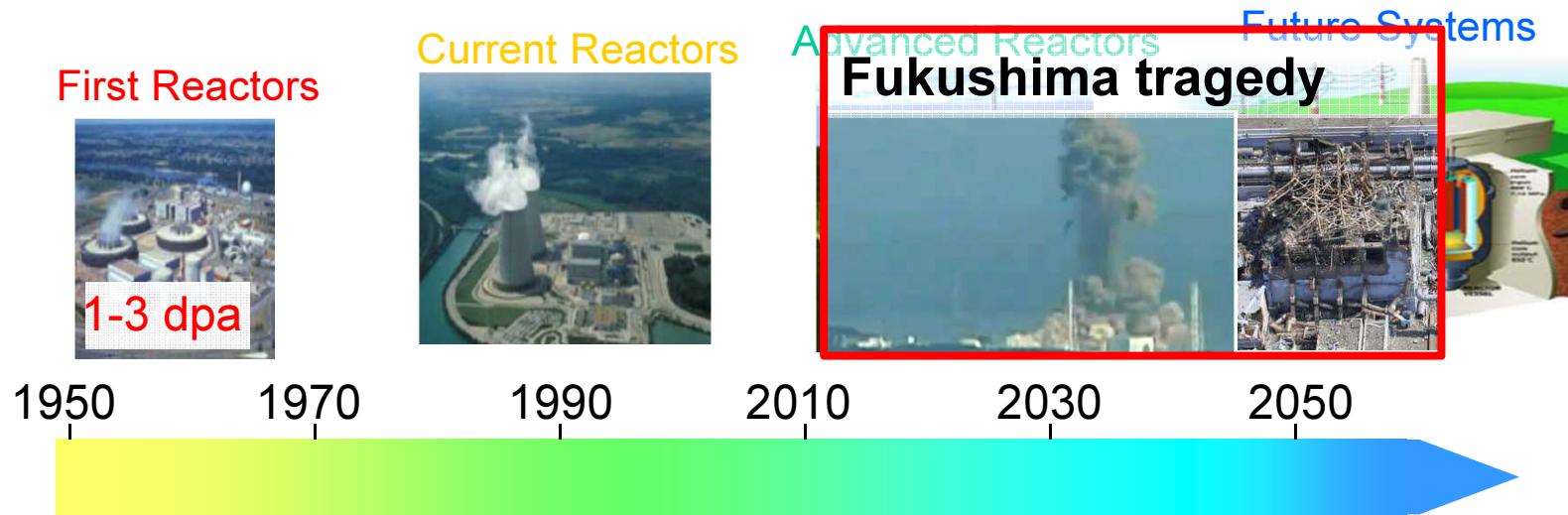
**A. Möslang**

**Institute for Applied Materials, KIT, Karlsruhe, Germany**

INSTITUT FÜR ANGEWANDTE MATERIALIEN - ANGEWANDTE WERKSTOFFPHYSIK (IAM – AWP)



# High Performance Materials for Energy



## Strategic Missions:

- Electricity, Heat, Hydrogen
- Environmental compatibility
- Cost effectiveness, sustainability

## **Safety first**

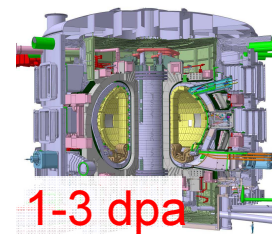
## Specific challenges for fusion:

- Short development path
- Loading more demanding (e.g H/He)

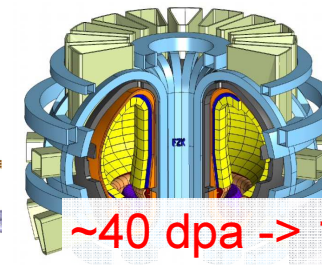
ITER IFMIF

DEMO

Power Plant



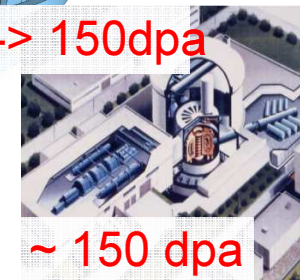
1-3 dpa



~40 dpa -> 150dpa



20-40dpa/year



~ 150 dpa

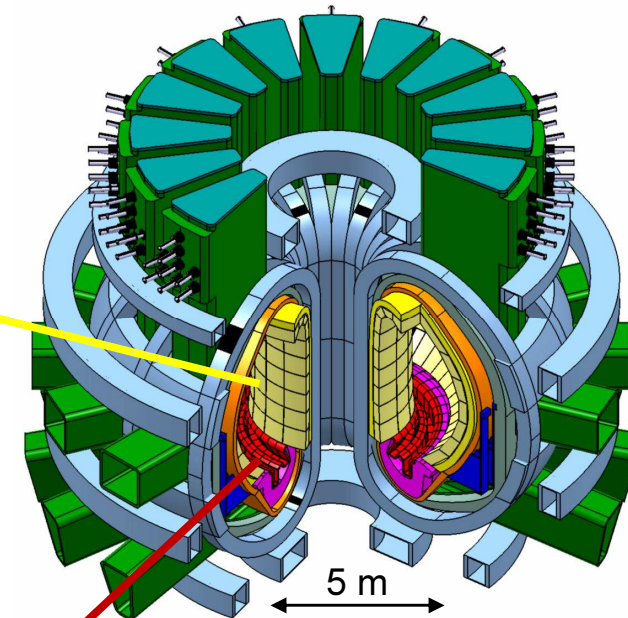
# Outline

- In-vessel materials: short overview and loading conditions
- - Ferritic-martensitic ODS steels (9Cr-YO)  
- Ferritic ODS steels (>13Cr-TiYO)
- Mechanical and microstructural properties
- Properties under neutron and ion irradiation
- Microstructure – property correlations
- Summary and Conclusions

# Fusion Power Plants: Material Challenges beyond ITER

## Blanket: $\leq 30$ dpa/yr, $\leq 2.5$ MW/m<sup>2</sup>

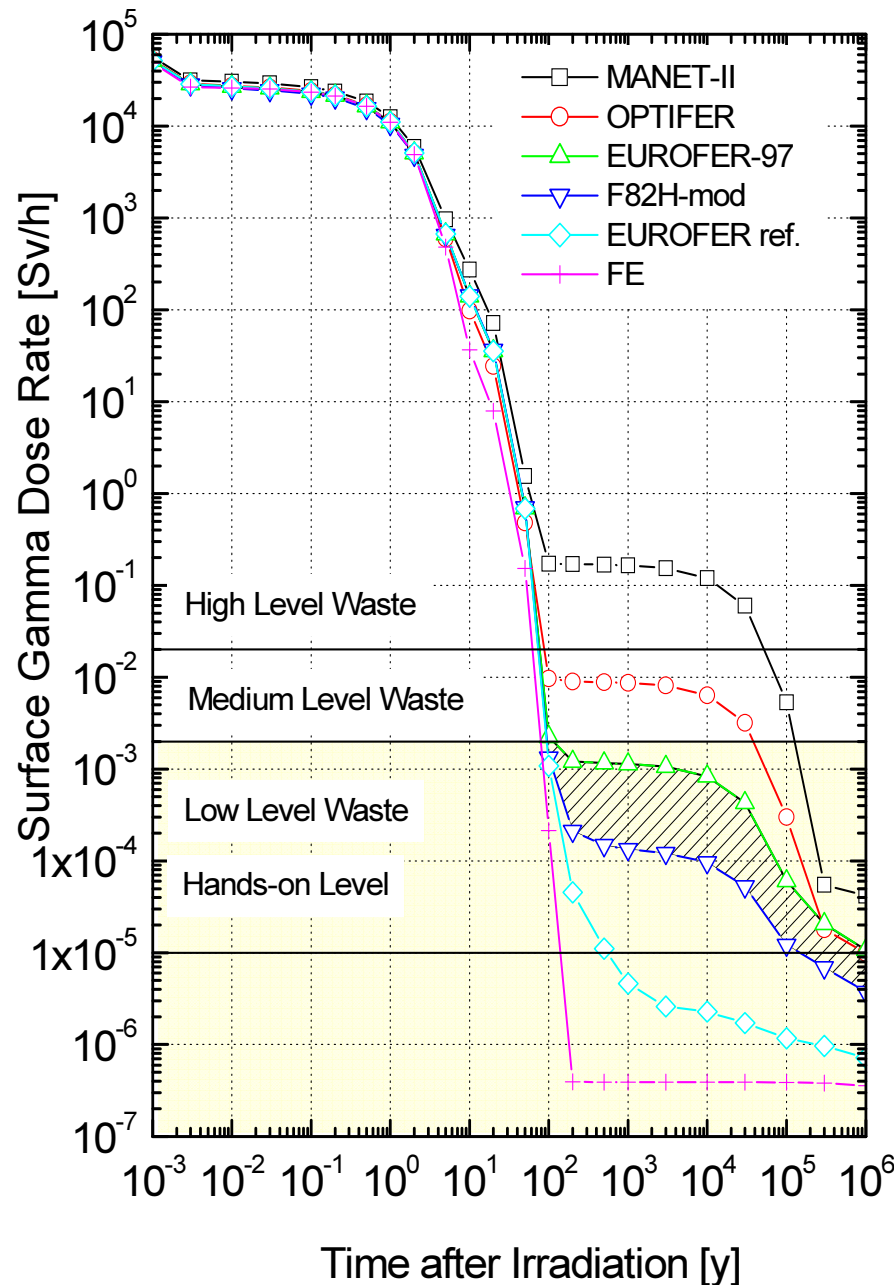
- Plasma Facing Materials
- Reduced Activation Structural Materials:
  - RAFM Steels (EUROFER, F82H) 350-550 °C
  - RAFM ODS Steels 300-650 °C
- Functional Materials
  - Neutron Multipliers (Be), Li ceramics
  - Diagnostics, Windows and Insulators



## Divertor: $\leq 10$ dpa/yr, 10-15 MW/m<sup>2</sup>

- Refractories (e.g. W-materials), others?  
850-1100 °C → ~600 - 1300 °C
- Nano-scaled RAF(M)-ODS Steels, others?  
350-650 °C → ~300 - 800 °C

# FUSION Priority: Low activation capability



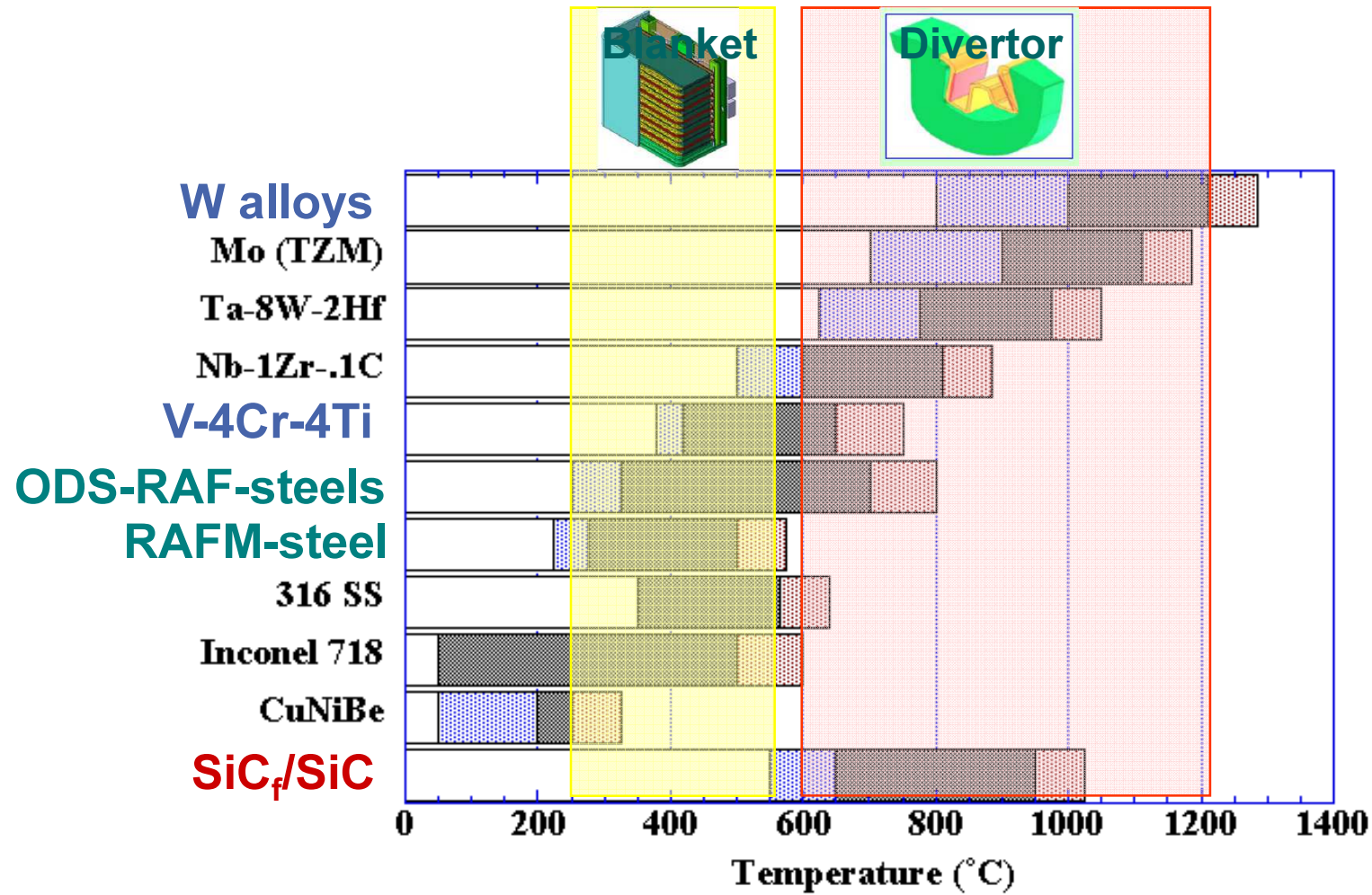
## RAFM 8-10%CrWTaV steels

- Substantial progress since the early 90-ies
- „Low level waste“ already after 80-100 years
- No “high level” waste disposal
- More than 60 tons produced in JA (F82H mod) and EU (EUROFER)

**The European reference steel EUROFER is presently characterized and code qualified (RCC-Mx)**

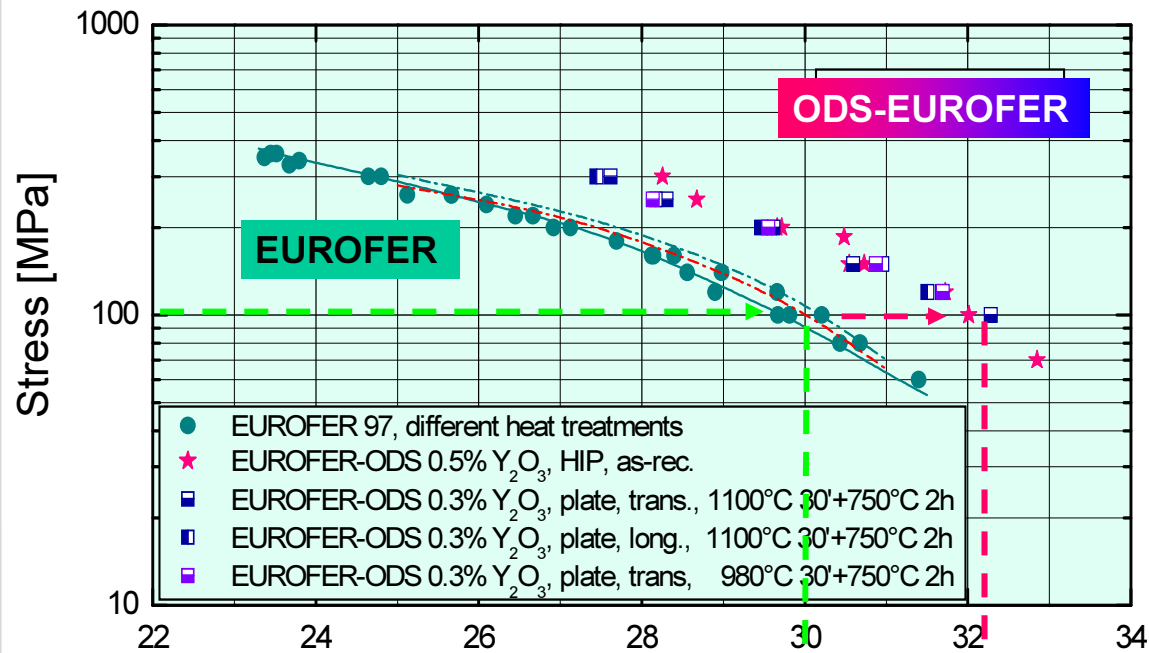
Long term irradiation  
(12.5 MWa/m<sup>2</sup>) of a  
DEMO reactor first wall  
Source: IMF I, FZK

# Application window of today's materials (~10 dpa)



# Long-term Creep Behavior: 100 MPa for $\geq 50\,000$ h

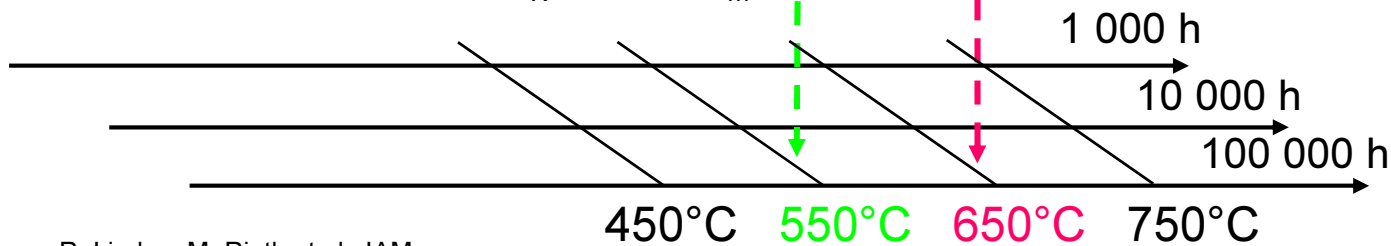
Master-Curve  
(Larson-Miller-Parameter)



## ODS-EUROFER (Fe-9Cr-1WVTa-0.3Y<sub>2</sub>O<sub>3</sub>):

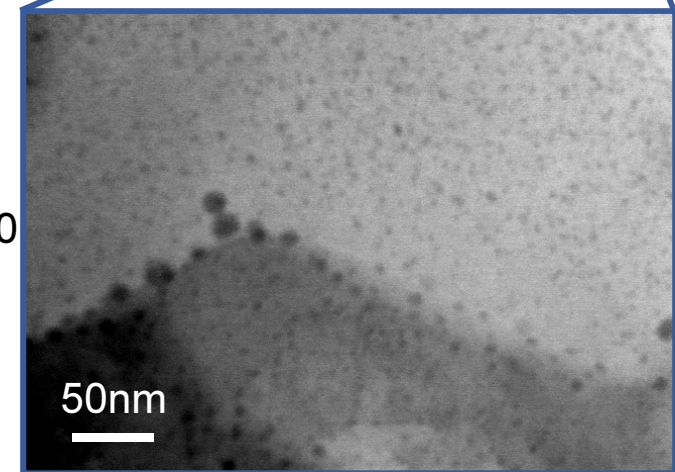
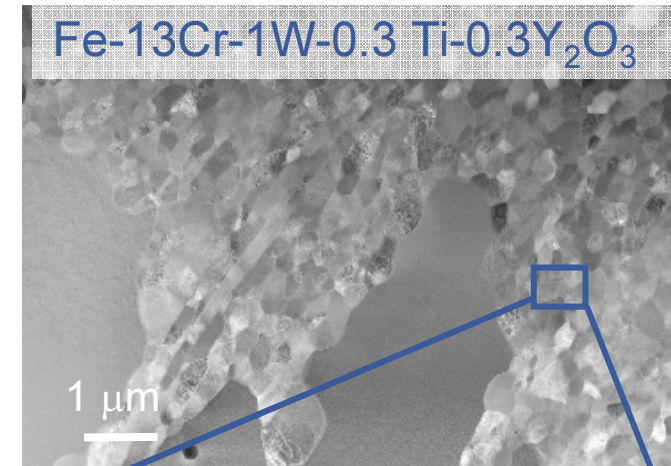
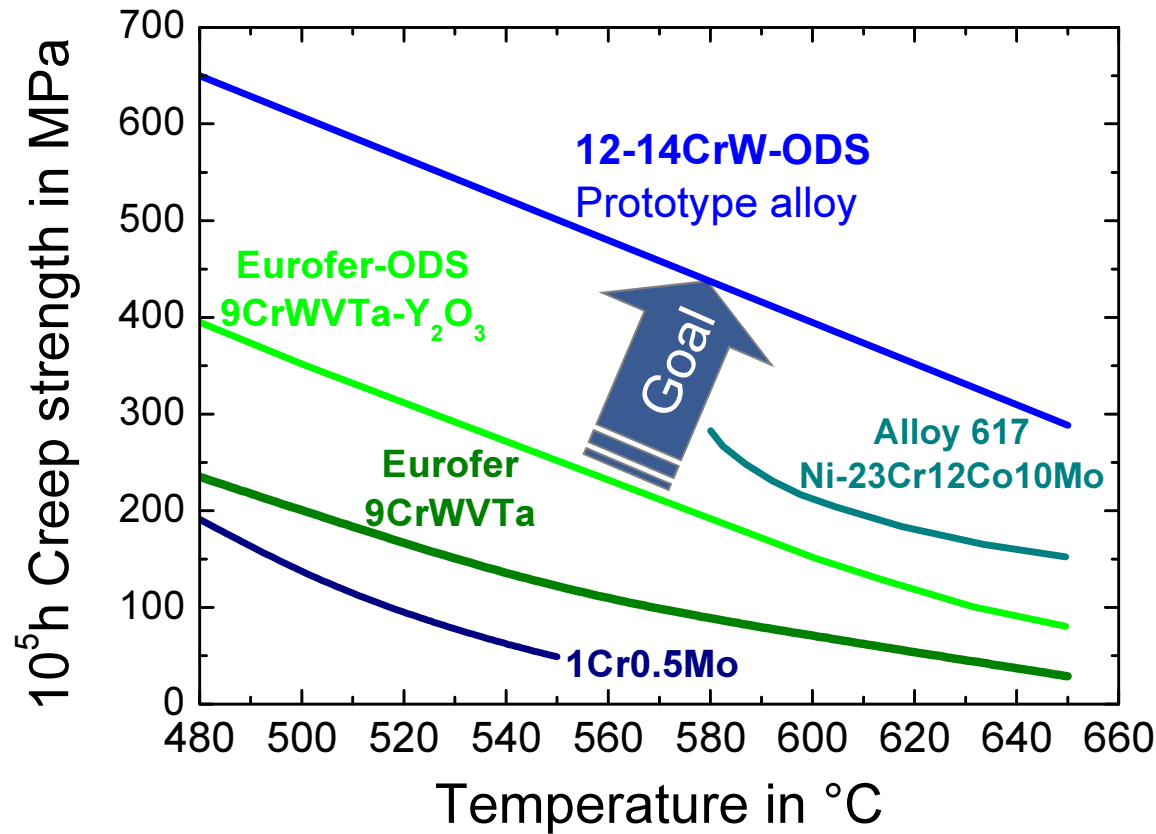
- Almost isotropic properties
- Several 50 kg batches fabricated with Industry
- Scalable technology
- T-window increased by  $\sim 100$  °C to 650 °C
- But: Can we do it better?

$$P = T_K (30 + \log t_m) 10^{-3}$$



R. Lindau, M. Rieth et al. IAM

# International challenge: Development of nanoscaled iron based “super alloys” (nanoscaled ODS steels)

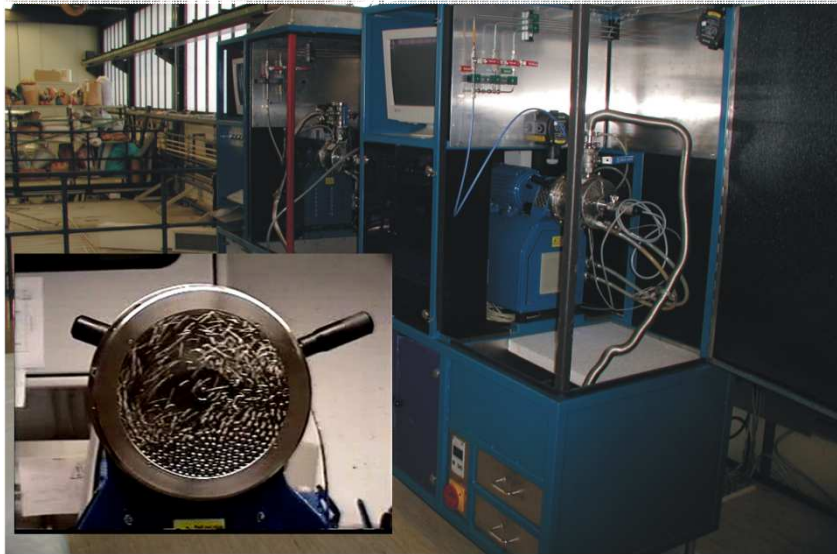


E. Eiselt, M. Klimenkov, R. Lindau, A. Möslang  
 J. Nucl. Mater 2010



# Fabrication process

## Mechanical alloying of powders



## Hot Extrusion



## Capsules after HIP

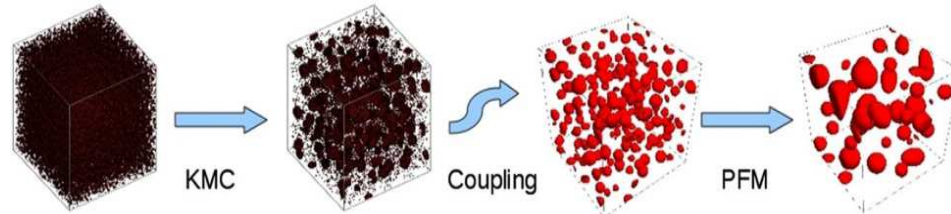


## Annealing + Hot rolling



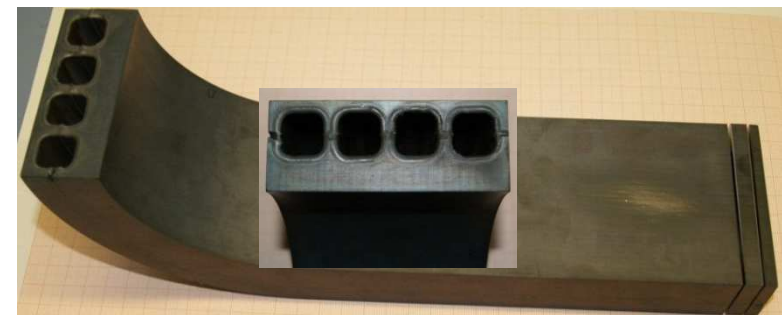
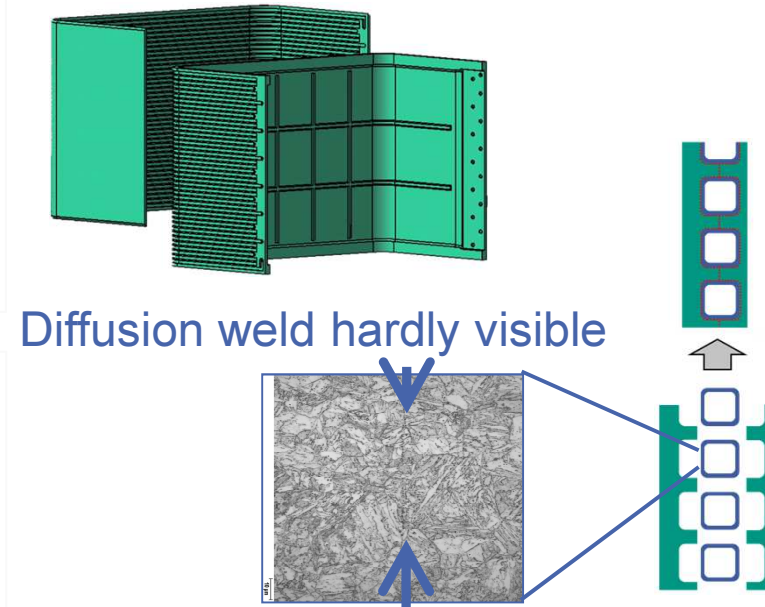
# Joining technology for ODS steels

TIG, EB and Laser welding not suitable:  
ODS particle coarsening above  $\sim 1250^{\circ}\text{C}$



## Diffusion welding successfully qualified

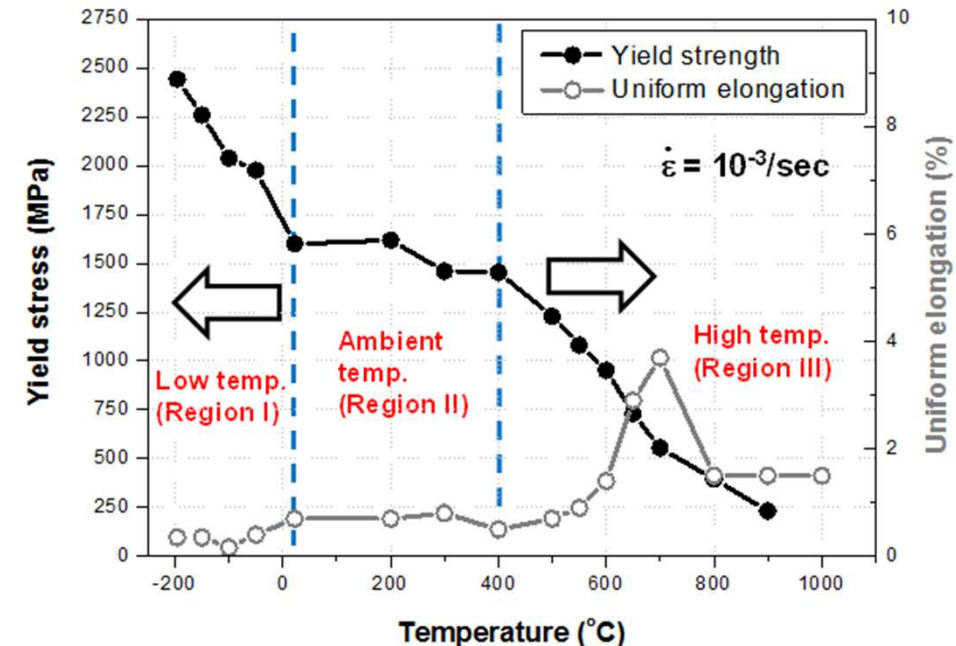
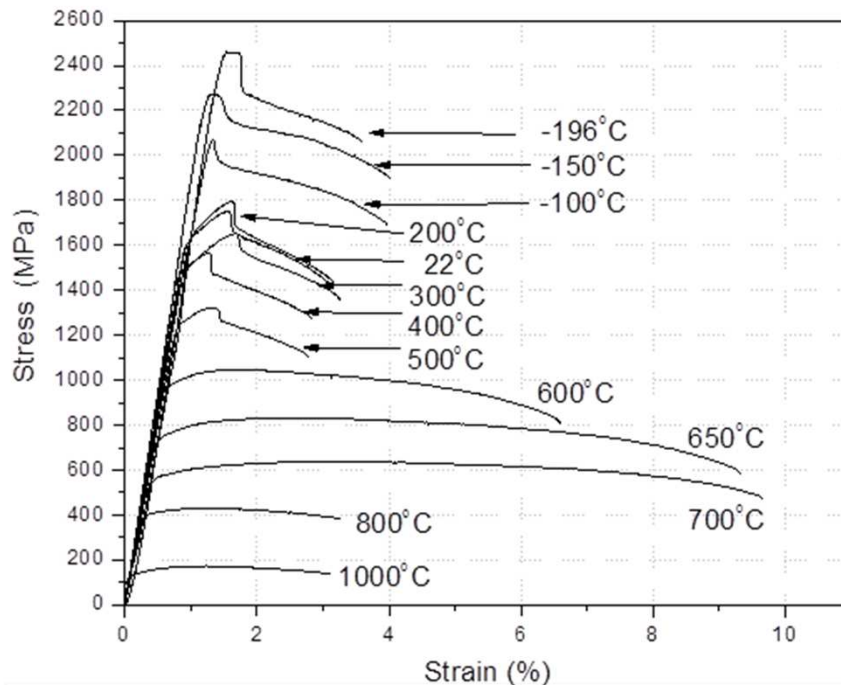
- E.g. as large scale FW fabrication method
- cost effective, robust and fail-safe fabrication route
- Compatible with industrial environment
- Tolerant against scattering of process parameters



M. Rieth et al, KIT

# Tensile properties of nanoscaled ODS steel 14YWT (Fe-14Cr-3W-0.4Ti-0.3Y<sub>2</sub>O<sub>3</sub>)

Courtesy of D. Hoelzer, ORNL

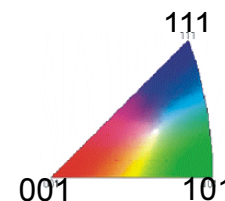
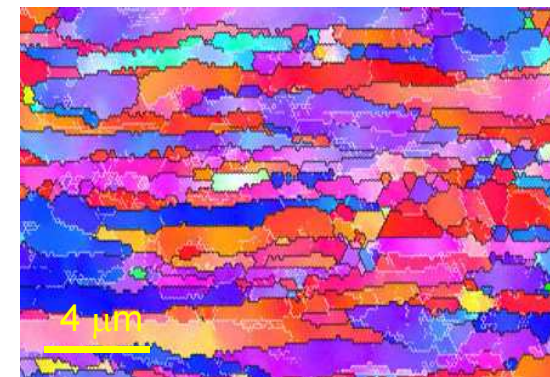
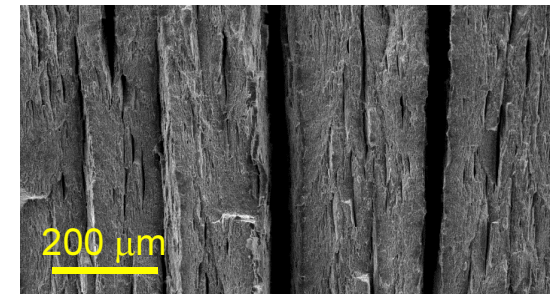
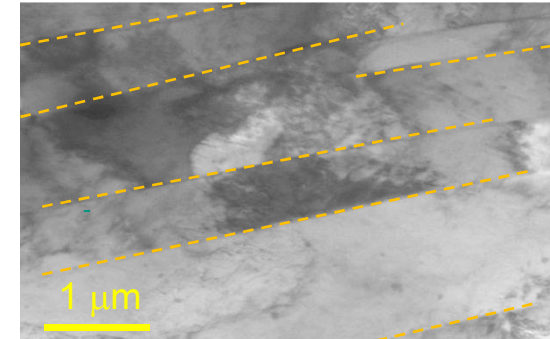


- ❑ Low uniform elongation, but extensive plastic deformation occurs after plastic instability until failure
- ❑ Ductile Brittle Transition well below room temperature (not shown here)

# Deformed ODS Steels: highly non-isotropic

**ODS steels:** Influence of hot rolling (~80% reduction) on properties

- Transmission Electron Microscopy (TEM):  
Rolling texture on microstructure
- Scanning Electron Microscopy (SEM):  
Fracture surface of Charpy tested samples shows clear fracture along texture, similar to Tungsten alloys  
J. Hoffmann et al., 2012
- Electron Backscatter Diffraction (EBSD):
  - Pronounced elongated grains
  - typical for textured microstructures  
ND:  $(001)\langle 110 \rangle$  and  $(111)\langle 110 \rangle$

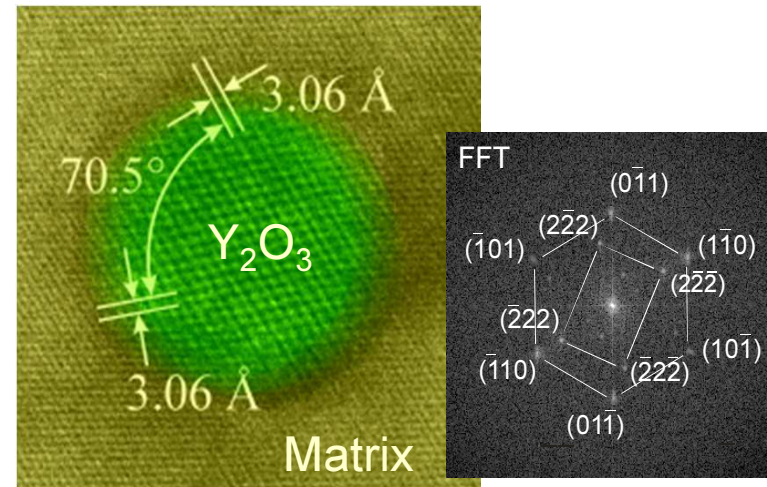


# Nanoscaled ODS Steels: High resolution TEM

$Y_2O_3$  particles (~4-15 nm):

- ❑  $(111)Y_2O_3 \parallel (110)FeCr$  - orientation of atomic planes; contradiction to classical text books
- ❑ Coherence despite of the high melting temperature (~2500 °C) of  $Y_2O_3$

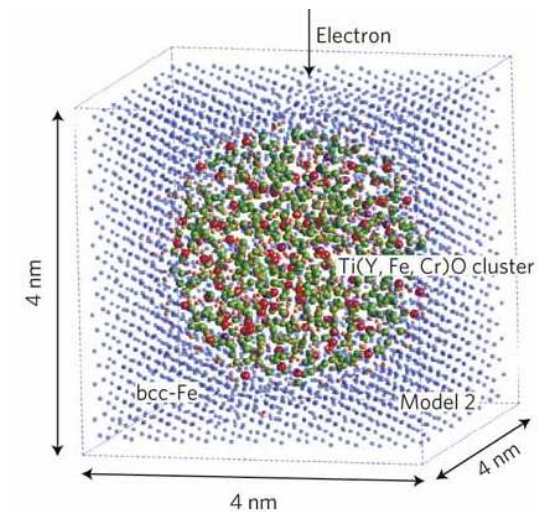
M.Klimenkov et al., J. Cryst. Growth 249 (2003) 381–387



Ti-Y-O particles ( $\leq 4$ nm):

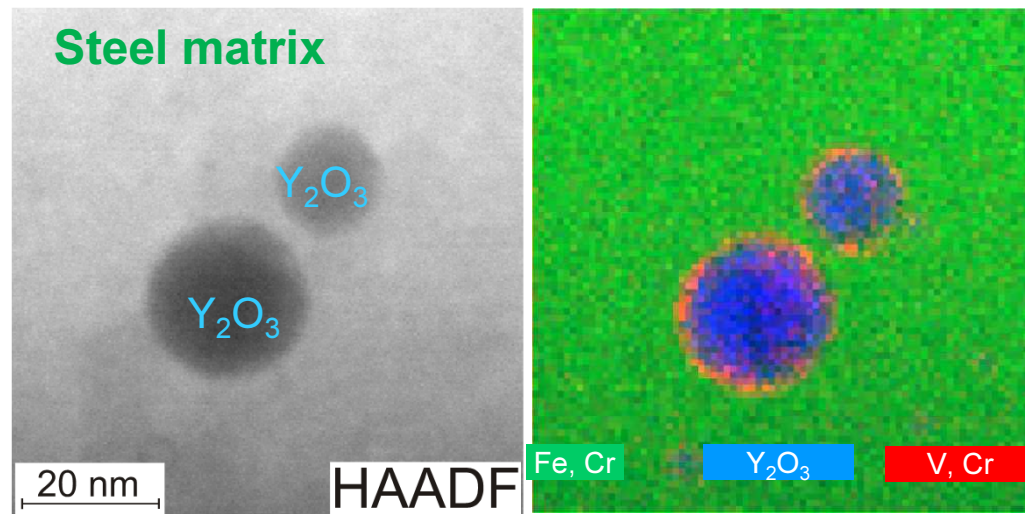
- ❑ Also bcc structure and still coherent
- ❑ But varying composition: Ti-(Y,Fe,Cr)-O

A.Hirata et al., NATURE MATERIALS 10 (2011) 922-926



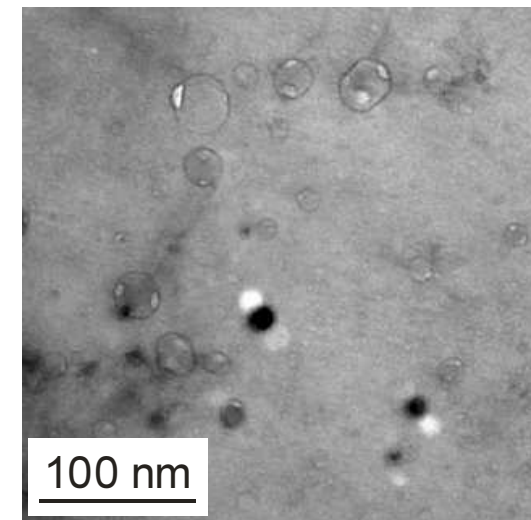
# Why nanoscaled iron based ODS-alloys have the potential for outstanding aging and irradiation resistance?

## Core shell structure



P. He, M. Klimenkov et al. J. Nucl. Mater. 428 (2012)131-138

## Trapping of Ar bubbles

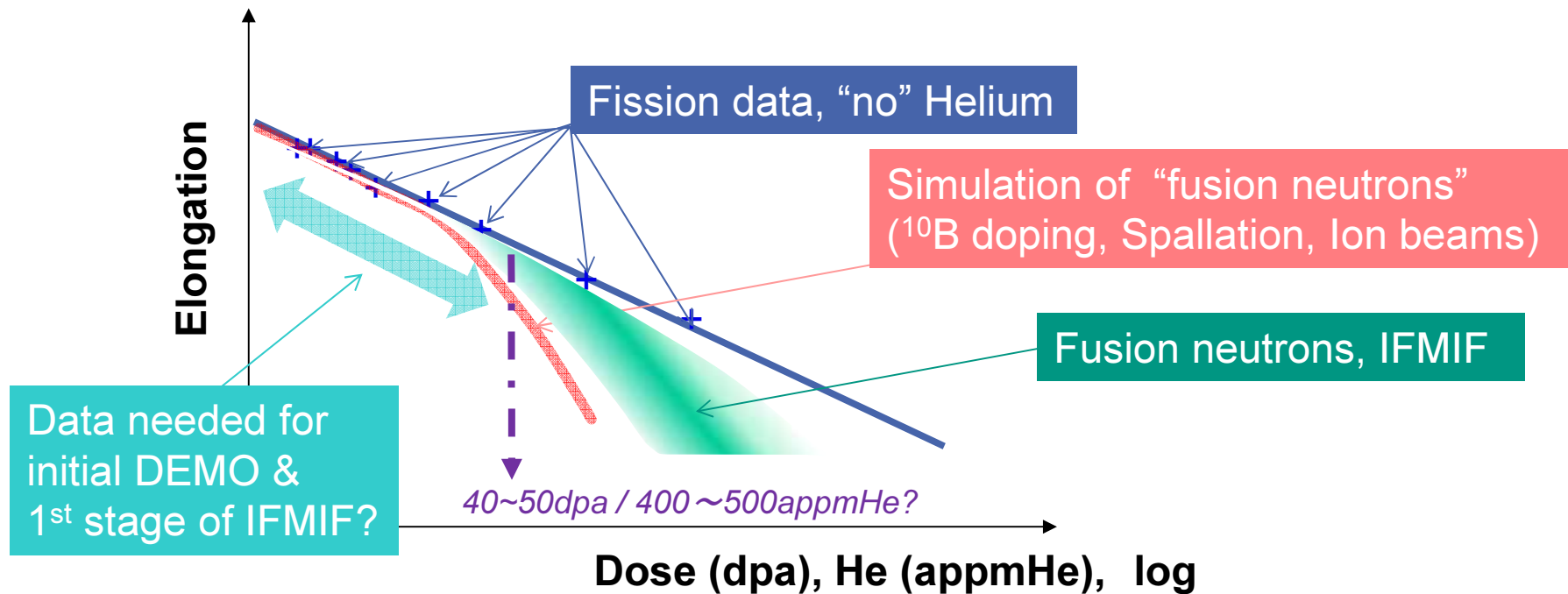


M. Klimenkov J. Nucl. Mater. 411 (2011) 160

- Interface Engineering”  
Nano-scaled ODS particles like  $Y_2O_3$  or  $Y_2Ti_2O_7$  are efficient trapping centers for diffusing alloying elements (Cr, V) and Ar.
- Outstanding perspectives, if also true for irradiation induced defects (vacancies, He)

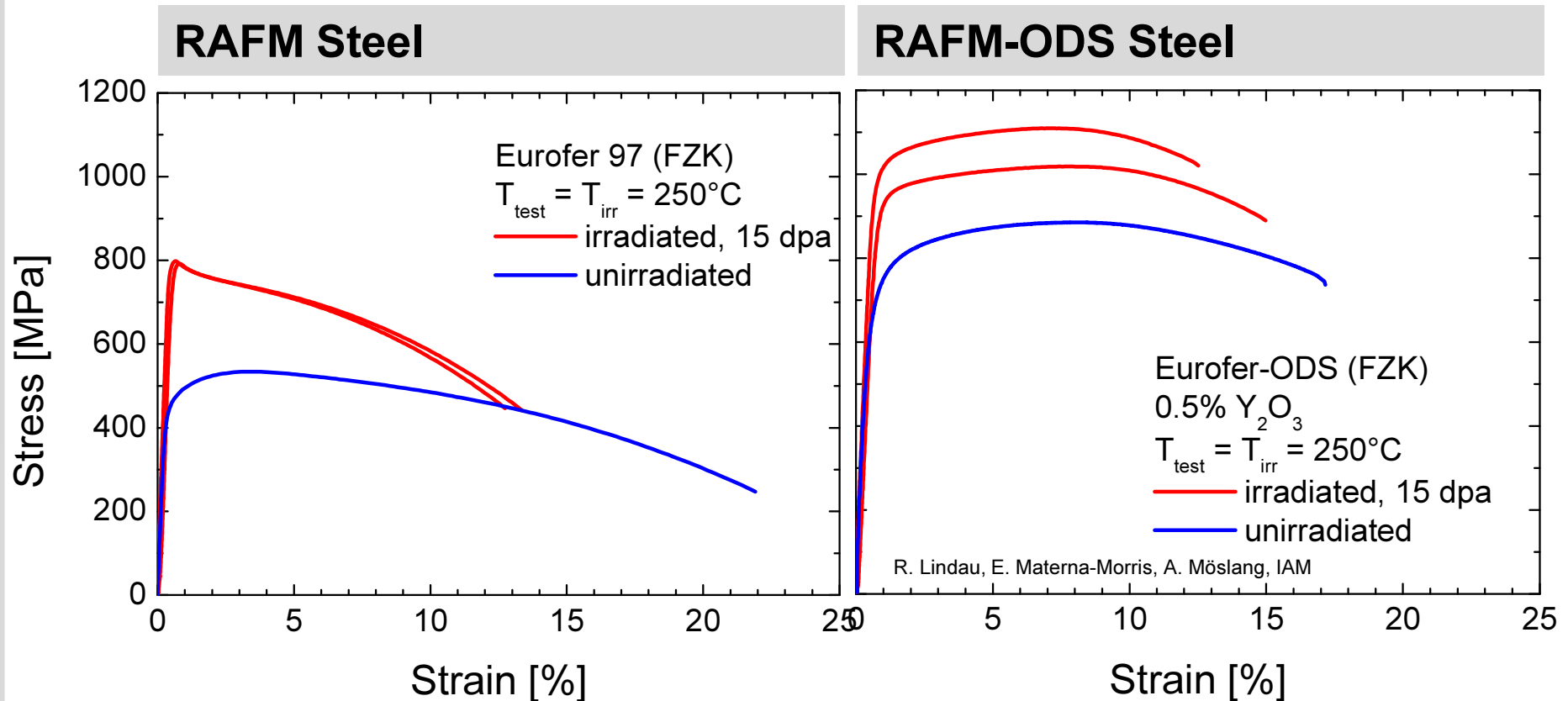
# Possible steps towards a fusion design code: Tensile properties as example

According to H. Tanigawa, E. Wakai



- Critical condition around 40~50 dpa / 400~500 appm He?
- This might be also the parameter window for initial DEMO and 1<sup>st</sup> stage of IFMIF and related design code development

# ODS EUROFER after Neutron irradiation: Substantial Improvement of tensile properties



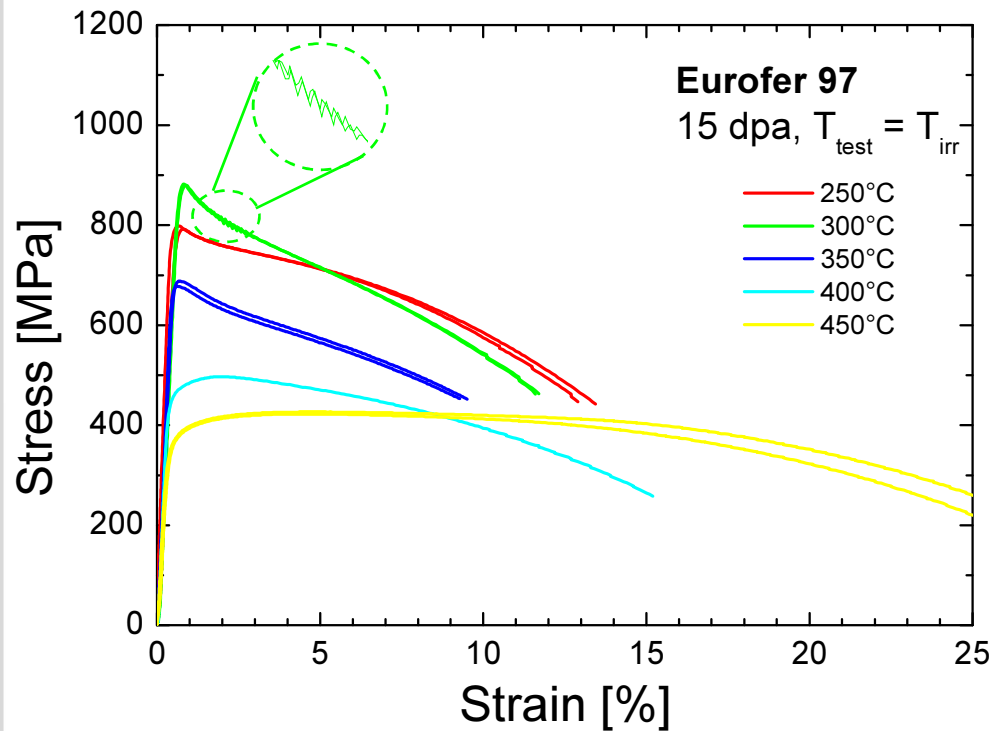
- ☹ Substantial irradiation hardening
- ☹ Early strain localization due to dislocation channeling →  $A_u \sim 0.3\%$

- ☺ Somewhat less irradiation hardening
- ☺ Still work hardening → almost no loss of uniform elongation ( $A_u \sim 7\%$ )

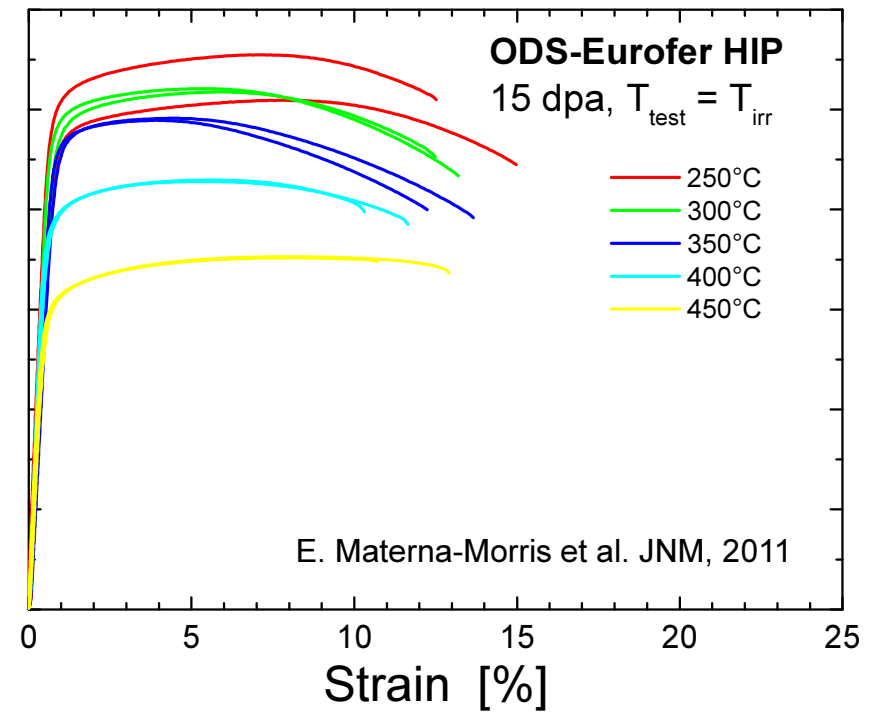


# ODS EUROFER after Neutron irradiation: Substantial improvement at all irradiation temperatures

## RAFM Steel

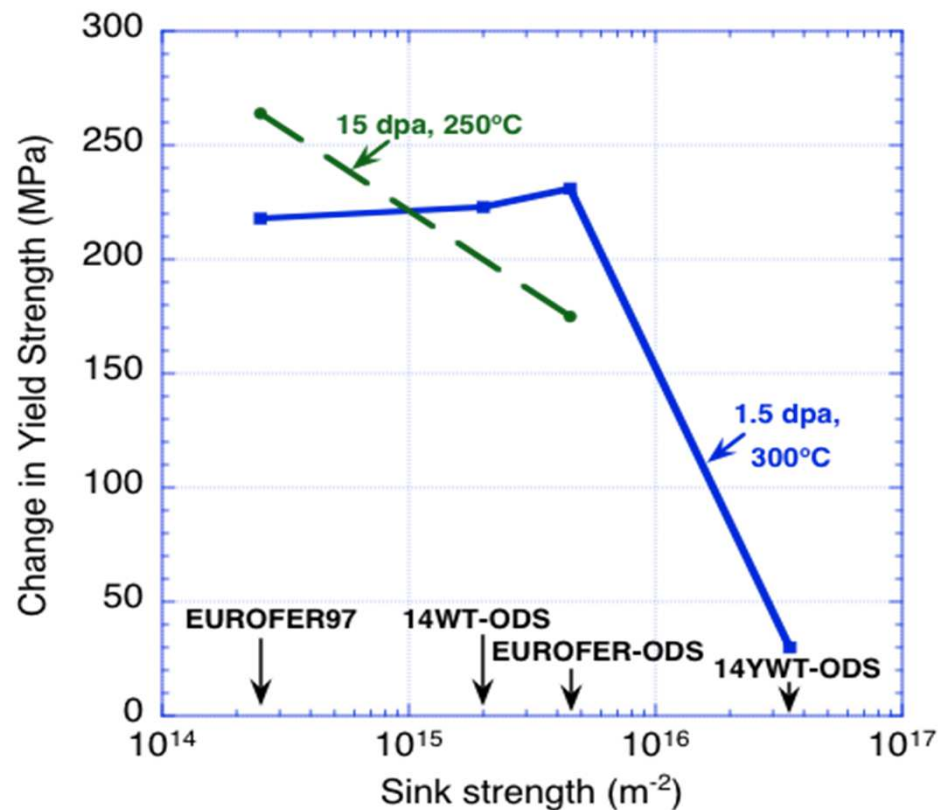


## RAFM-ODS Steel




# Neutron irradiation of ODS steels:

Tensile strength vs. sink strength (density of ODS particles)



S.J. Zinkle, A. Möslang, T. Muroga, H. Tanigawa;  
 Nucl. Fusion **53** (2013) 104024 -104037

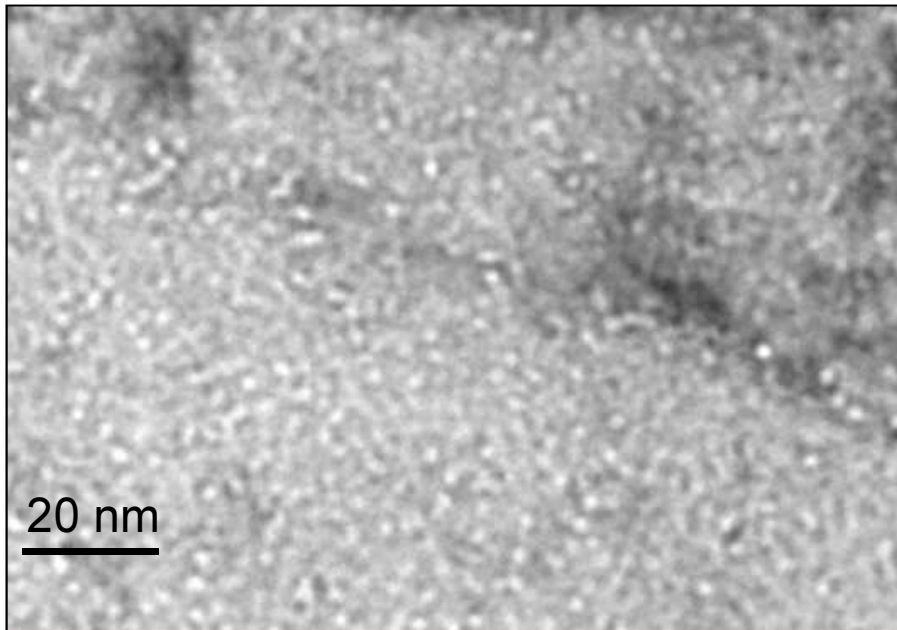
The irradiation tolerance increases substantially with ODS particle density  
 defects are trapped at particle matrix interface and recombine

# ODS steels: He trapping at particle-matrix interface

KIT  
Karlsruhe Institute of Technology

## 14YWT (14Cr-3W-TiYO)

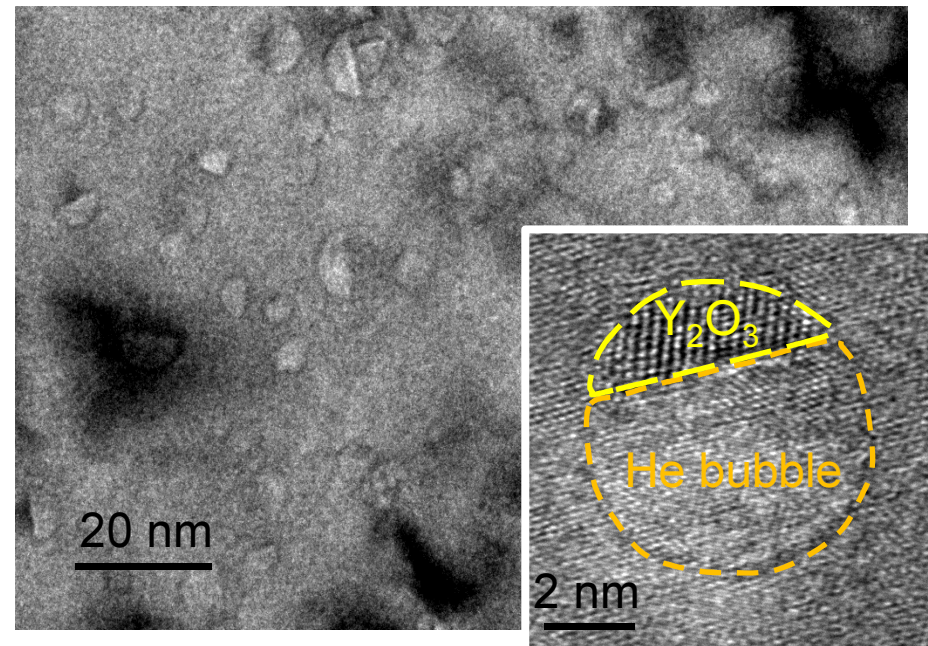
- irradi.  $\text{Fe}^{3+}$  (6.4 MeV),  $\text{He}^{++}$  (1 MeV),
- 2200 appm He, 650°C



Courtesy of D. Hoelzer, ORNL

## EUROFER-ODS (9CrWVTa-YO)

- $\text{He}^{++}$  (30 MeV),
- 1000 appm He, 550°C



A. Ryazanov et al., J. Nucl. Matter 442 (2013)153-157

Effective He trapping indicates: ODS steels may be extremely irradiation tolerant

# Summary and Conclusions

- Significant progress has been made in the fabrication of ferritic nanoscaled ODS Steels
  - The powder metallurgy based production route is practically established
  - near term step are medium sized heats (10-50 Kg range)
- The mechanisms responsible for high-temperature strength and creep behavior are emerging
- Scientific understanding of structure-property relationships advanced
- Nanoscaled ODS steels have the potential for extremely high aging and irradiation resistance at high service temperatures and fit perfectly into an energy efficient landscape